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SECOND REPORT OF THE AD HOC GROUP OP SCIENTIFIC EXPERTS TO CONSIDER INTERNATIONAL CO-OPERATIVE MEASURES TO DETECT AND IDENTIFY SEISMIC EVENTS

Appendices

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APPENDICES TO CHAPTER 3

APPENDIX 3.1

Technical instructions for extracting Level 1 parameters **at seismic stations**

In this appendix a detailed description is given of how Level 1 data should be extracted from SP and LP instrument recordings at stations of the global network. Reference is made throughout to parameters specified **in Tables 3.1 and 3.2. By necessity, this appendix is written in a rather technical language, and the reader is referred to Chapter 3 of CCD/558 for a non-technical description of the basic principles involved,**

A3.1.I General specifications

(i) Time

Most modern s.eismograph stations maintain a timing accuracy of 0.1 seconds; however, it may become temporarily more uncertain. In that case the timing uncertainty should be reported. Because of the high accuracy of time measurements the problem of instrumental time delays must be noted. For WSSN-SP instruments at 1 Hz: phase delay time is about 0.3 s, group delay time is about 0.4 s.

- **(ii) Seismographs are roughly divided into two classes;**
	- **1. Short period (SP) instruments having peak response at periods of the order of 1 second or less;**
	- **2, Long period (LP) systems with peak response at longer periods, up to** 30 **s or more; long-period instruments are here taken to include also those generally termed medium-period or broad band.**

Note, however, that modern digital broad band stations have the capability of extracting signals in both the SP and LP bands.

(iii) Seismic noise is measured in the different period ranges corresponding approximately to the frequencies of main seismic signals, i.e., on records of SP seismographs (T = 0.2 - 1.0 s) and on records of LP seismographs $(T = 2 - 8 s$ and $T = 10 - 30 s$, **respectively). All measurements are made in the section of the recording preceding the first arrival.**

A3.1.2 Standard parameters reported by participating staitiens from short-period vertical seismographs

1 . First arrival

On a visual record first arrivals are defined by a certain change in amplitude or phase. The time reading, after- being corrected, is given in hour, minute, second and tenth of a second in Universal Coordinated Time (UTC), , Some stations may be able to report one-hundredth of a second. If the applied time correction is uncertain (clock problems) by more than +0.1 s it must be reported in qualitative remarks. The first arrival should always be identified, if possible, by one of the standard symbols. The symbols (phase codes) used by the Interantioanl Seismological Centre are recommended.

2. First motion sign and clarity

The clarity of the phase should be denoted by i if it is readable to an accuracy of at least ^{\pm}0.2 s, and by e if it is more uncertain, between **-(0,2 and l.O) s. Note that e and i denote the accuracy of the timing rather than the character of the recording which may depend on the paper or film speed. If the uncertainty in the onset of the first arrival is** greater than ^{\pm}1.0 s, (e) should be used.

Direction (or sign) of the first motion on the vertical SP and LP components (C or D, Ü or R) shouTd be reported (see also subitem 23 below). In cases of complicated wave patterns (small onsets followed by large onsets) the first visible motion is read. Do not report the direction if in doubt. If possible the first motion on the LP horizontal components should also be reported. First motion notations;

- **С short-period compression**
- **D short-period dilation**
- **U long-period compression**
- **R long-period dilation**
- **V long-period movement on the NS component, direction to the North (the code N cannot be used because PN would then be ambiguous)**
- **Y ibid., direction to the south**
- **E** *E-VI* **component, direction to the east**
- *VI* **ibid., direction to the west.**

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The clarity index precedes the phase identification, the first motion index follows it. The first motions from SP and LP instruments do not **need to agree.**

3. P-wave amplitudes

Ground amplitudes A_i of the first phase are to be determined from **maximum trace amplitudes using the instrument's response curve. Trace amplitude is measured as the center-to-pealc deflection from the median** line or may be obtained by halving peak-to-trough deflection of symmetrical **waves,**

The ground amplitudes are reported to a precision of 0.1 nanometers (i.e., 10~^^ meters). Since the upper limit for an absolute calibration of seismographs is 5**-**105**^? it is understood that the amplitude cannot he measured with a better accuracy. The amplitudes for the first phase should be measured to the maximum deflection within the intervals, 0-6 s, 6-12 s, 12-18 s and 18-300 s, according to the duration of the wave group.**

4. Associated times

The time associated with each reading of amplitude and period is reported; it shouli he measured as illustrated in Figure АЗЛ.1. - -

5. Associated periods

Periods corresponding to each A_i are measured at zero crossings or **between two neighboring peaks or troughs. Periods should be read to one-tenth of a second.**

6. Seismic noise amplitude

The maximum noise amplitude at a frequency close to that of the signal should he measured and converted to ground amplitude in nm. This amplitude is measured within 30 **seconds before the first onset and reported for each event.** The signal-to-noise ratios can then be determined using A_i , (sub-item 3) at **data centers.**

7. Noise period

The period corresponding to the maximum noise amplitude is measured in a way similar to that described under 5.

8. Secondary phases

A standard notation for all phases is that used by the International Seismological Centre. Arrival times of identified hut also clear unidentified secondary phases should be reported. Hour is reported only if it is not the same as the hour of the preceding phase. Identification of phases is more confidently carried out at date, centers; however, advantage should be taken of experienced interpreters at individual stations. For the clarity i or e are used. Measurements of arrival time, maximum recorded amplitude and corresponding period of secondary phases follow the same rules as mentioned under 1, 3> 55 however, only one maximim amplitude is measured. It is important that among secondary phases pP and sP are reported.

9. Complexity

10. Spectral moment, ratio or vector

There are no standards for calculating the parameters under 9 and 10. Before a universal agreement is reached, it is recommended that stations computing these parameters should describe the procedure they use. Note that the complexity and spectral ratio parameters will be reported only by certain stations of specialized capabilities within the global system.

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13.1.3 Standard parameters to be reported from short period horizontal seismographs

11. Phase identification and arrival time of the 0 wave

The time is reported to 0.1 s.

12. Clarity of the 3 phase

Reported as 1 if readable to an accuracy of 1.0 s or better, as e otherwise. Note the S phase onset is seldom, if ever, legible to within the + 0.2 s required for using clarity index 1 for P-vaves.

17. Haximum amplitude of short period S

Neasured within the first 10 seconds of the S wave for both the NS and E^{η} components. The respective arrival times should not differ by more than one half signal period, so that the amplitudes can be combined vectorially.

A. Corresponding arrival time Reported for both components in hours, min, s.

15. Corresponding period Reported to 0.1 s precision.

15. Secondary phase descriptions Reported as under item 8.

AJ.1.4 Additional standard parameters from arrays of short period vertical seismographs

This category of parameters concerns arrays of vertical short period seismographs, including arrays of digital broad ban seismographs with short period filtering capability.

Each array station reporting the following parameters $(17, 18, 19, 20, 21)$, should publish a description of its procedures of determining these quantities before standardized guidelines are elaborated. The parameters nos. 17 and 18 will be used for locating events at the data centers, using an agreed travel-time

derivative table for this purpose, it is therefore not essential for each array station to produce and report the parameters under 19 and 20.

17. Apparent slowness

Determined with the precision 0.1 s/deg. At medium aperture arrays the slowness and direction of an arriving P wave could be obtained as a least gouares fit of arrival times, or time differences, to a wave front. It can also be obtained vith lover accuracy by fixed search programs.

13. Epicenter azimuth and distance

Reported to 0.1° or to the accuracy that is judged to be realistic in each case. Note that the asimuth corresponds to the station to epicenter direction.

19. Epicenter latitude and longitude

The epicenter coordinates should be reported to 0.1° or to the accuracy that is judged to be realistic in each case.

20. Origin time

Estimated and reported as hours, minutes, seconds.

21. Ilagnitude

Whenever epicenter distance is known, magnitudes will be determined using the vertical component short period P waves and the procedure recommended by the IASPEI Commission on Practice (Appendix 3.2).

A3.1.5 Standard parameters to be reported from long-period seismographs

Reporting should preferably be grouped by event, rather than by instrument and readings of a particular phase from different instruments should be grouped together.

Long-period $P - vertical component$

22. Phase identification and arrival time

Phase identification, arrival time and clarity (i or e) should be given even if a short-period initial arrival is reported. In order to avoid separate reporting of long-period arrival times being treated as a new event if different from short-period arrival time, one must indicate that the same arrival is referred to. (Grouping of the reportings for the same event would usually take care of this.)

23. First-motion sign and clarity

The comments under 2 apply here. Note that first-motion readings are desirable also on the LP horizontal components.

24. Maximum amplitude A_M

For long-period P , only one amplitude measurement (the maximum one) is required. Reporting precision is 1 nm.

25. Arrival time corresponding to A_M

Reported to a precision of 0.1 seconds.

$26.$ Period corresponding to $A_{\rm M}$

Reported to a precision of 0.1 seconds.

27. Noise amplitude AN

The maximum noise amplitude is measured within 1 minute before the first onset on the vertical component, converted to ground amplitude in nm and reported for each P-wave reading. Period range 2-8 seconds.

28. Period corresponding to A_N

The period in seconds corresponding to the maximum noise amplitude is reported.

29. Secondary phase description

See subitem 8.

Long-period S - horizontal components

30. Arrival time

Phase identification and arrival time (to a precision of 1 second) are reported for one component.

J1. First-notion clarity

See subitem 12.

22. Jaximum amplitudes A_I

Heasured separately on each horizontal component, within the first 40-60 seconds of the S wave. The neasurements should be carried out at times differing by no more than one half signal period.

 \mathbb{R} . Arrival times corresponding to each \mathbb{A}_{Π}

Reported for both components in hour, min, s.

14. Period corresponding to each A₁

Reported to 0.1 s precision.

35. Secondary phase description

Reported as under item 8.

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Rayleigh waves - vertical components

36**. Arrival time of LR**

The onset time of LR is hard to read and the clarity is strongly dependent **on signal-to-noise ratio. The onset time is specified to the nearest second, hut must usually he considered very uncertain.**

37. Maximum amplitude A_M

Amplitude of the maximum deflection is measured on the vertical component and reported in nm.

38**. Arrival time corresponding to A^^**

Indicated in hour, min, second.

39_^ Period corresponding to A^

Reported to a precision of 1 second.

⁴⁰**. Other maxima A (LR) X-----------------***m a x-— -*

Maximum amplitudes A^^(LR) with periods of 10, 20, 30 **aлd** 40 **seconds** $(vithin \pm 10\%)$ on the vertical component; reported in nm.

4 1 **. Times of the maxima A (LR) ü------------------------ max-—** *i-*

Times are given corresponding to the four different maxinia, with a precision of 1 second.

42_; Corresponding periods

The actually observed periods of the other maxima of LR waves are reported in seconds.

43» Seismic noise amplitude, A^^

Largest amplitude of seismic noise x^ith period between 10- 30 **seconds is measured on the vertical component within 5 minutes of the section of the record preceding the event. The ground amplitudes in nm are reported.**

44» Noise period corresponding to A^

The period is reported to .a precision of 1 second. Note, however, that the long-period noise may he irregular and it is often difficult to determine the period accurately.

Love waves - horizontal components

45. Arrival time of_LQ,

Reported to a precision of 1 second on one of the horizontal components. Note that in the same way as for LE (item 36**), LQ onsets are hard to determine accurately.**

46**. Maximum amplitudes A^^**

Maximum ground amplitudes of LQ on the NS and EW components are reported **in nm. The respective time of measurements should not differ by more than one half signal period.**

47. Arrival times of

The respective times of $\Lambda_{\rm M}$ on the two components are reported to a **precision of** 1 **second. •**

48**. Periods corresponding to Aj^**

Reported for each horizontal component; precision 1 second.

A3.1.6 Additional standard parameters from arrays of long-period seismographs

49. Apparent slowness

Reported for the vertical component of the P-wave only. Precision 0.1 s/deg, see also no. 17.

50 **. Azimuth**

Azimuth can be determined not only for large arrays with digital recordings, but also for small arrays by measuring the time difference on and analog recording between the arrivals of the same wave peak in a wave **train at all stations (this applies also to No.** 49**). The parameter helps to associate LP with SP data.**

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51. Surface wave magnitude M

Magnitude based on vertical LR waves determined using the procedure recommended by the IASPEI Commission on Practice, precision 0.1 unit. Measurements should be made directly from amplitude and period without application of station corrections.

52. Magnitude M_{SH}

Magnitude M_{CFT} based on short or long period horizontal component S. measurements is determined.

A3.1.7 Qualitative remarks

local events)

It is very important that the report is accompanied by remarks of the experienced analyst qualifying, if possible, the character of the event as seen from the visual inspection of the record or by a more sophisticated analysis. The following remarks are suggested:

Local: event judged to be within approximately 150 km of the station. Regional: event judged to be within approximately 800 km (excepting

Quarry blast: event announced by responsible authorities as a quarry blast, total charge in tons and coordinates should be indicated if known; events having a record typical for blasts according to the analyst's experience should be also indicated by 'possibly quarry blast' even if no official announcement is available.

Rock burst: event announced by authorities or qualified to this category by a typical wave pattern.

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Mixed events: two events overlapping and causing some confusion in reading an interpretation; if possible, they should be identified (local, distant, etc.).

Multiple (double) event: complex wave pattern particularly in the P-wave group justifying such statement according to the analyst's experience.

- Deeper than normal, intermediate: qualification made by the analyst if the wave pattern and amplitude ratios of main phases warrant it.
- Uncertain time: if the time correction is uncertain by more than \pm 0.1 because of clock problems.

The above parameters are transmitted within double parentheses according to the International Telegraphic Seismic Code (see Chapter 4**).**

АЗ.1 **.В Signal duration PUR and local magnitude**

In case of local and regional events, these parameters, as measured on short period recordings, may he reported as well as amplitude and period,

A3.1 .9 **Doim-time information**

It is very important to keep records of the time intervals when a station has been out of operation, and such information should be communicated when applicable.

Illustration of rules for measuring wave amplitude, period Figure A3.1.1 and time of maximum oscillation (a), kinematic and dynamic parameters of SP records (b) and spectral parameters of LP records (c).

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aPPENDIX 3.2

Instructions for measuring amplitudes and periods for magnitude determination from observations at regional and teleseismic distances

LASPEI COMMISSION ON PRACTICE SUBCOMMISSION ON MAGNITUDE **Revised draft, September 1978**

Note; These instructions have been included only as a reference to ongoing ' standardization work in the seismological community, and should not he interpreted as necessarily representing the views of the Ad Hoc group

The determination of earthquake magnitude is based on observations of amplitude A and period T of seismic waves. It is essential for subsequent earthquake studies to report the time that an observation of A and T is made.

The amplitude of a seismic signal on a record is defined as its deflection from the base-line. It is important that A, T, and the time of the observation should he measured for' each of the phases P, S, and L waves.

For many phases, and particularly surface waves, the record is symmetrical about the base-line and amplitude may be determined either by direct measurement from the base-line or by halving the peak-to-trough deflection. **For phases that are strongly asymmetrical the amplitude should he measured as the maximum deflection from the,base-line.**

The amplitude and period from the vertical component is the most important. If horizontal components are available, readings from these should also he reported. They should be measured at the same time on the record so that the amplitudes can be combined vectorially.

The period T corresponding to the amplitude A is measured in seconds between two neighboring peaks, or two neighboring troughs, or ideally from trace crossings of the hase-line,

P-Waves

The P-wave amplitude measured should be that of the maximum trace deflection usually within the first 25 **seconds of the first onset, hut this interval may he extended up to** 60 **seconds for large earthquakes recorded on hroad-band** **CD/43/Add.l page l6**

instruments. When more than one component is available, the amplitude **from each should be reported separately.**

The observation time should always be measured as the time to the first **peak or trough of the trace cycle being measured. This need only be estimated to the nearest** 1 **to** 2 **seconds.**

The amplitude measured on the record should be converted to ground motion in nanometers using the amplitude-period response curve of the instrument, When several instruments of the same type operate at the same station or when several instruments of different frequency response are-available, the amplitude and period from each should be reported separately.

S-Naves

The measurement of amplitudes and periods on the seismograms is performed as described above. It is recommended that if possible the beginning of the S-wave be checked against travel-time tables. The amplitude and period should be selected in the interval up to 4**O-**6**O seconds after the beginning of S-waves.**

L-Waves

The measurement of amplitudes, periods and times of observation on records is performed as described above for the maximum deflection and for the largest amplitude in the 17-23 second period range of the surface wave **train.**

The measurements for horizontal components should he carried out at the same time of arrival allowing for a difference of less than one period.

For large earthquakes when mantle waves are often recorded, amplitudes and periods bf the vertical and horizontal components with the period of about 200 **seconds should also he measured.**

The observations of A and T for all phases mentioned above should be included in station reports. Itg is essential in reporting such observations that the type of instrument used is clearly stated. For this, the classification given in the 'Manual of Seismological Observatory Practice' may be

used. Broad-band instruments are preferred for all measurements of amplitude **and period.**

Note: Seismograms can be very complicated and, ultimately, the selection **of a particular measurement must he left to the observer's experience.**

Instructions for measuring amplitudes and signal durations for magnitude determination of local earthqualces

Amplitude measur'ëments

Por local earthquakes, i.e., those where the S-P interval is less than 2 minutes recorded on short-period instruments, it is not always possible to measure the period of seismic waves so the maximum trace.deflection (converted to ground motion) and time of observation should be reported.

Duration measurement

For local earthquakes, stations should report the signal duration defined as: the time in seconds between the first onset and the time the trace **never again exceeds twice the noise level which existed immediately prior** to the first onset. Very often local earthquake recordings will cause **high-gain, short-period instruments to saturate, thereby making an amplitude reading impossible even for small seismic disturbances. Therefore, to provide the data with which to derive relations for duration magnitudes that are based on signal amplitude magnitudes, both types of observations should be made on as many of the same earthquakes as possible.**

As with regional and teleseismic data, the type of instrument and where possible the period of the peak of the response curve used should be- clearly stated.

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APPENDIX 3.3

Example of a bulletin from a seiamic station

Table A3.3.1 shows a possible format of a seismic bulletin and at the same time gives an example of how it should be completed when processing a **recording of a strong seismic event. The format of a special bulletin used at seismic stations in the USSR has been used as the basis. In the proposed global system, the time period covered by each bulletin wculd normally he one day. The table should he considered only as an example, and further.work is required for the development of a final bulletin format-**

Each sheet of the bulletin carries the name of the station, the month and year, the number of the bulletin (bulletins are numbered in sequence for each year)' and the page number. In addition, the time interval of the reporting period, the geographical co-ordinates of the station and its altitude above sea level are entered on the first sheet of each bvilletin.

In column 1, the numbers of all the seismograms are given (a single numbering **system is used for all types of instruments installed at the station). If no earthquakes are identified in the seismogram, the words 'No earthquakes noted' are entered under the seismogram number.**

In column 2, the serial numbers of the recorded seismic signals in the **seismograms are listed. Signals are numbered in sequence during each year.**

In column 3, the date of each signal is shown.

In column 4, the type of wave recorded and the first-motion sign and clarity **are given. If the type of wave is not precisely determined, the designation of the wave is placed in brackets. Clear first motion is designated by the letter 'i' and an mclear first motion hy the letter 'e'. In the event of first arrival of the signal, the first arrival sign is indicated, A '+' sign corresponds to upward motion (compression phase) on the vertical component and to N and E on the horizontal components; a '-' sign corresponds to downward motion (dilatation phase) on the vertical component and to S and W on the horizontal components.**

In column 5, the abbreviated designation of the instrument and of the component for which the wave arrival time is determined are given.

In' column 6 , the wave arrival time (hour, \sin uinute and second) is given. The precision of measurement of the arrival time is to 0.1 s with an SP instrument and to 1 s with an LP instrument.

In column *7 ,* the single (O-P) amplitude of the recorded oscillation in the wave in question is θ hown in millimeters. The mesurement precision with an SP instrument is to 0.1 mm and with an LP instrument to 1 mm.

In column 8, the displacement amplitude for the wave whose recorded amplitude is shown in column 7 is given in nanometers. The precision of measurement is to 0.1 nm.

In $\frac{\text{column } 9}{\text{column } 9}$, the period for the wave amplitude indicated in column 7 is shown in seconds. The precision of measurement for body-wave periods by both SP and LP instruments is to 0.1 s and for surface waves with LP instruments to 1 s.

In column 10, the noise amplitude for the instrument and component in question IS shown in nanometers. The precision of measurement is to 0.1 nm.

In column 11, the noise period is shown in seconds, with precision to 0.1 s for an SP instrument and to 1 s for an LP instrument.

In column 12, the apparent velocity determined for P and LR waves is given in km/s, with precision to 0,1 km/s.

In column 13 , the azimuth from the station to the epicenter of the event is shown in degrees, with precision to 0.1 degrees.

In $column 14$, the epicentral distance is shown in degrees, with precision to 0.1 degrees.

In column 15, the value for the magnitude $m_{\tilde{h}}$ is shown in the line where the value of the maximum P-wave amplitude recorded with an SP instrument **СТ/43/Add.l page 20**

(vertical component) is entered; the value of magnitude M_{SH} in the line where the value of the S-wave A_{M} recorded with an SP instrument (horizontal component) is entered, and the value of magnitude M_A in the line where the **value of the L-wave** A_M **recorded with an LP instrument (vertical component) is entered. The magnitude values are detennined with precision to 0.1 units.**

In columns 16 and 17 the values of the co-ordinates of the epicenter latitude $(\cancel{0})$ and longitude $(\cancel{\lambda})$ - are given in degrees, with precision to **0.1 degrees.**

In column 18, the time at the focus when the event originated (hour, minute, second) is given with precision to 1 s.

Column 19 is provided for analyst remarks. If possible, the type of the event recorded ('local earthquake', 'quarry explosion', 'mixed with another event', etc.) should he indicated under this heading.

Columns 1 to 11 contain data compulsory for all types of stations, and columns 12 to 18 data which can be obtained only at type-III stations.

Table A3.3.1

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BULLETIN No.

From 22 September OO hrs to 23 September OO hrs 1978
Seismic station "

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 $\begin{array}{l} {\mathbb{C}} \mathbb{D} \mathbb{Z}/7 \mathbb{Z} \rightarrow 1 \\ {\mathbb{C}} \mathbb{D} \rightarrow 21 \end{array}$

APPENDICES TO CHAPTER 4

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APPENDIX 4.1

Proposed Coding formats for Level 1 data

This appendix gives a detailed description of the proposed transmission format for Level 1 data. It is intended to supplement the International Seismic Code published in the WMO Manual on Codes, Vol. I, as a special appendix. Since the proposed Level 1 format is an extension of that Code, only features which are new in relation to the Code are described. An example of the full text of a Level 1 report for a strong earthquake recorded at an array station is included. Note that this example represents maximum processing in the case of a major seismic event. In most cases, *however,* the text will be considerably shorter, and will only provide data on the P wave recorded on a vertical short-period seismograph.

Description of the format

The proposed format, which is described in detail in Tables A4.1.1 through A4 .1.4} is in most respects identical to the International Seismic Code. However, the following deviations should be noted;

1. Numbering

The messages originating from each national facility will be consecutively nmbered starting at the beginning of each calendar year. The general form of the number is Nyn where N is a prefix, y is the last digit of the calendar year and n is a number of 1 to 5 digits. (The present code allows for a maximum of 3 digits). 2. Additional phase identifiers

As described in detail in Tables A4.1.1 and A4.1.2, several new phase identifiers will be needed compared to tbe International Seismic Code. Each of these is to be followed by the corresponding arrival time, period and amplitude in accordance with standard practice. Note that all the amplitudes of these new phases will be quoted in nanometers (nm).

3 . Identifiers for parameters

Again referring to the tables A4.1.1 and A4.1.2, a number of new identifiers corresponding to specific computed parameters will be needed.

4. Later phase information

Por each later phase, the maximum amplitude (quoted in nm) and corresponding period that is associated to the phase will be reported. (This is not currently provided for in the International Seismic Code.) Por horizontal instruments the component on which the measurements were made might be specified as a suffix (E or N) immediately following the phase identifier. However, care must be taken not to exceed the maximum length (5 characters) of a phase identifier.

Additional comments

5» Grouping of readings

Readings from short and long period instruments for the same phase should he grouped together. When the time of arrival is determined more accurately on the SP instrument, the arrival time on the LP instruments need not be given, but the long period maximum amplitude identifier should be followed as usual by its associated arrival time, period and amplitude.

6. Reporting interval

The time interval covered by the transmitted message should be specified in a, comment field as e.g.,

 $((BEG$ APROl 120000 END APRO2 120000)).

Note: In case of a station transmitting a group of messages, e.g., once per day, the first message may contain the reporting interval for the entire group. If so, the number of messages (NM) in the group should be included as, $e.g.,$

 $((DEG APROI 120000 EID APRO2 120000 N17)).$

7. Down-time information

If a station has been out of operation, this time interval should be reported in a comment field as OUT (date, time) followed by TO (date, time). This reporting should be made as soon as possible after the station is back in operation. Example: $((0 \text{UT} \, \text{SEPO2} \, 191530 \, \text{TO} \, \text{SEPO2} \, 223515)).$

Additional explanation may be included in the brackets as found necessary. Concluding remarks

'In conclusicn the changes needed in the International Seismic Code in order to accommodate the envisaged data exchange are;

- expansion of the numbering field (item 1)

 \sim addition of some 30 new allowable identifiers (items 2 and 3)

- allowing for amplitude/period information to follow later phases (item 4). In addition, a number of new phase codes would be needed to allow for horizontal component specification (item 4). Likewise, the reporting of direction of first motion of horizontal components (Appendix 3.1, item 2) would necessitate several new allowable phase codes.

Items 6 and 7 above have in this proposal been included as comments, and will thus not necessitate any change in the established format. However, it would be desirable to agree upon a format in which these items could be reported using specific identifiers, and this should be given further study.

It is emphasized that the coding formats proposed here will need to be agreed with other users of the WMO/GTS and also approved by the WMO prior to implementation in the proposed data exchange. Further revision may therefore be necessary.

Table A4.1.1.

Proposed identifiers for Level 1 short period parameters

Table $A4.1.1.$ (cont.)

* Form employed in the International Seismic Code should be used.

** Each phase identifier is followed by arrival time, period (T) and amplitude (A) according to standard conventions.

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Table A4.1.2

Type Proposed οf Component Parameter Identifier Wave: $\rm P$ (a) Standard parameters -Vertical stations of types I, II and III. 22. Arrival time $\frac{\Delta \mathcal{L}}{\Delta \mathcal{L}}$ 23. First-motion sign and $\frac{1}{2}$ clarity 24. Maximum Amplitude, $A_{\overline{M}}$ MLP** 25. Arrival time corresponding to $A_{\mathbb{M}}$ \mathbf{r} 26. Period corresponding to $A_{\rm M}$ NLPA 27. Noise amplitude, A_{IJ} 28. Period corresponding **NLPT** to $\Lambda_{\rm N}$ 29. Secondary phase description: Amplitude Period Arrival time Δ^{\prime} S Horizontal 30. Arrival time $\frac{2\pi}{\sqrt{3}}$ 31. First-motion clarity 32. Maximum amplitude, $A_{\overline{M}}$ on each horizontal component 35. Arrival times MSLPE, MSLPN** corresponding to each $A_{\mathbf{M}}$ 34. Periods corresponding to each $A_{\tilde{d}}$ 35. Secondary phase description: Amplitude ⊹ Period 꼮 $\frac{\Delta \mathcal{L}}{\Delta \mathcal{L}}$ Arrival time

Proposed identifiers for Level 1 long period parameters

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Table АЛ.1.2 (cont.)

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 $\frac{M}{N}$ **Form employed in the International Seismic Code should be used.**

 $\mathcal{H}^{\mathcal{M}}_{K}$ **Each phase identifier is followed by arrival time, period (ï) and amplitude (A) according to standard conventions.**

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TABLE A4.1.3

Example of a telegraphic text transmitted from an array station for a large earthquake

SEISMO N82351 ((BEG SEP22 180000 END SEP23 180000 NMS)) ARR SEP22 IPCU 1919020 M1X19035 T3A60 M2X19112 T3.2 A53.1 M3X19160 T3.5A29.8 M4X19233 T3.5 A27.2 MLP19060 T6A144 NT1.0 NA5.1 NLPT8 NLPA15 E PP 2247 T3.6A18.2 T8 A108 ES 30025 MSE 30080 T4A75.2 MSN 30080 T4A61.0 MSLPE 30090 T9A216 $\sim 10^{-10}$ MSLPN 30090 T9A135 ESS 3711 T4.7A61.7 T12 A192 IRZ 4841 MIR5407 T22A271 HIL5637 T10A135 M2L5311 T20A200 M3L5203 T30A105 M4L5012 T40A98 NLFT20 NLPA12 LQ 4251 MLQE4302 T21A220 MLQN4302 T21A172 CMPX 23.02 SPMM 2.45 SLO 4.8 AZ226 DIS94 LAT-35 LON-120 OT190541 MB6.5 SIOLP 4.8 AZLP221 M56.4 MSH6.6

 $\sim 10^{-10}$ k

STOP

Table A4.1.4

Explanation of the text in Table A4.1.3

identification of type of data (seismic) SLISMO $N32551$ - message no. 2351 during 1978 for the station(s) (\sqrt{BEG} SEP22 180000 END SEP23 180000 MM8)) \cdots This is the first message in a group of 8 covering the time interval indicated (UTC). ARB station name SEP22 - date of recorded event (22 September) IPCJ 1919020 - first-motion clarity (I), type of wave (P) , direction of first motion (C - compression on short-period seismograph; U - compression on longperiod seismograph), arrival time (19h19m02.0s) in component Z MLL19055 - time of arrival (19m03.5s) for P-wave first amplitude, A_1 , in component Z T3ACO - period (3 seconds) and amplitude (60 nm) for amplitude A_1 in component Z M2X19112 "3.2A53.1 - time of arrival, period and amplitude for amplitude A_0 in component Z M3X19160 T3.5A29.8 - time of arrival, period and amplitude for amplitude A_{z} in component Z 14A 5255 13.5427.2 - time of arrival, period and amplitude for amplitude A_A in component Z MLF19060 T6 A144 \cdot time of arrival, period and amplitude on LP seismograph, component Z. 1.T1.C NA5.1 - period and amplitude of noise on short-period seismograph, corponent 7. NUTFe, NEPAL5 - pariod and amplitude of noise on long-period seismograph, component Z E FP 2247 T3.5418.2) -- time of arrival, periods and amplitudes of secondary T8 A108 longitudinal PF wave in component Z (on short and long period instruments, $respectively)$ ES $:0025$ - first-motion clarity (E), wave type (S), arrival time, (component not indicated) MSE 30030 T4A75.2 - time of arrival, period and amplitude for maximum amplitude of short period S wave in component E Men 30080 T4A61.0 - time of arrival, period and amplitude for maximum amplitude of short period S vave in component N ISILE 30000 T9 A216 - time of arrival, period and amplitude for maximum amplitude of long period S-wave (component E)

ISLPH 30090 TJ A135 - time of arrival, period and amplitude for maximum amplitude of long period S-wave (component N)

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Table $A4.1.4$ (cont.)

E SS 3711 T4.7A61.7) - clarity and time of arrival, periods and amplitudes for secondary shear phase (SS) (component not indicated) $LRZ4841$ - time of arrival of Rayleigh wave in component Z $MLR5407$ T22A271 - time of arrival, period and amplitude of maximum phase in Rayleigh wave in component Z IIL15637 TIOA135 - time of arrival and amplitude in Rayleigh wave for 10 second period in component Z M2L5311 T20A200 *) ~* arrival times and amplitudes in Rayleigh wave for, $M3L5203$ T30A105 \langle respectively, 20, 30 and 40 second periods in M4L5012 T4OA98) component Z ИТ20 NA12 - amplitude of noise for 20-second period on long-period vertical seismograph LQ 4251 - time of arrival of Love wave in component E 1ILQE4302 T21A220 - time of arrival, period and amplitude of maximum phase in LQ wave in component E MLQN4302 T2IAI72 - time of arrival, period and amplitude of maximum phase in LQ wave in component N CMPX 23.02 - 'complexity' parameter in P wave recording SPIM 2.45 - 'spectral moment' parameter for P *waves* SLO 4.8 - apparent slowness (s/degree) $AZ226$ - azimuth from station to epicenter (degrees) DIS94 - epicential distance (degrees) LAT-35 - latitude (degrees) of epicenter $($ - south) LON-120 - longitude (degrees) of epicenter $(-)$ = vest) OTI9054I - origin time (l9h 05® 41s) MB6.5 - magnitude, determined for short-period P *wave* SLOLP 4.8 - apparent slowness of long period P (s/degree) AZLP 221 - azimuth to epicenter from LP recordings (degrees) MS 6 .4 - Rayleigh *wave* magnitude on LPZ seismograph MSH 6.6 - S-wave magnitude on long-period horizontal seismograph STOP - end of communication
APPENDIX 4.2

A study by the WMO on the routing and transmission of seismic data (level 1) over the World Neteorological Organization Global Teleommunication System (WMO/GTS)

Background for the WMO study

Before presenting the study by the WMO, we give below a brief introduction and a description of the input data provided for the study by the Ad Hoc group. In the Ad Hoc group's report CCD/558, four examples of seismic networks were considered, each corresponding to a different assumption regarding the availability of stations. Each network was restricted to 50 short period (SP) and 50 long period (LP) stations.

Table 4.2.I lists the stations included in at least one of the four networks. The possible routing of Level 1 data through the GTS circuits is indicated for each station.

For the present study, it was considered desirable to get an assessment of the GTS routing of data from all of these stations but without having to make a separate study for each network. Therefore this study considers all stations taken together. The resulting 'network' of 76 SP and 76 LP stations is of course larger than any of the network examples and the conclusions of the study would be interpreted accordingly.

For example, the stations of this extended 'network' in North America and Europe are essentially those of Network I. The corresponding load on the regional GTS circuits would therefore be similar to what would happen if Network I were implemented.

On the other hand, for South America and Africa, the 'network' stations are essentially those of Network III. Therefore, the study of the line capacity in these areas would mainly be relevant for Network III and Network III (SRO).

The expected volume of data reported from each station is highly dependent on the seismic activity, which varies considerably from one day to another. The input to this study was taken to be a 'high' activity day, i.e. a volume of data that would typically occur only a few times per year. Information obtained from the experts of the Ad Hoc group indicated that a reasonable

estimate of such a load would be: 50 earthquakes for each station during a 24-hour period, 20 of which would be large enough for long period parameters to be reported.

At stations which employ an automatic detector there is the possibility of false detections being generated. It is at present not possible to accurately assess the volume of data generated by such false detections, but it is assumed here that this volume will be small in comparison to that generated by real events. This question does, however, merit further study.

We assume that each event is reported as a separate telegraphic message, and that the average length of each message is as follows (station designations refer to Table $4.2.1$):

The WMO study is now presented.

Routing and transmission of seismic data (Level 1) over the World Meteorological Organization Global Telecommunication System (WNO/GTS)

According to the information available from the Ad Hoc Group of Scientific $1.$ Experts to Consider International Co-operative Measures to Detect and Identify Seismic Events, seismic data from stations of 50 different countries will have to be transmitted over the CTS. Each type of seismic station and the volume of data expected to be transmitted from each type of station, as well as number of each type of station, are as follows:

This volume will not be constant and will on the average be much lower. However, it is assumed that the total daily volume of seismic data to be transmitted over the GTS would reach 1.159.000 characters.

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2. In order to develop the routing arrangements for handling the required seismic data, the volume of data to be inserted by each GTS center and time **required for transmitting data over the GTS circuits have been estimated.** Table 4.2.2 shows the volume of data to be inserted by each GTS center as well as routing on the GTS, transmission speed and time in this respect. The routing **arrangements have been developed taking into account the present routing of meteorological information on the GTS as prescribed in the Manual on the GTS,** Each center on the Main Trunk Circuit (MTC) is responsible for collecting **seismic data from the originating centers as listed in the table.**

3* It should be noted that certain circuits might not he able to accommodate the required seismic data due to the heavy traffic of meteorological information which is already transmitted over the circuit concerned. Furtheimore, some GTS centers which are not connected directly to a center on the MTC will transmit seismic data via other GTS centers. Therefore, the centers responsible for relaying information from other centers to the MTC center will handle a large **amount of seismic data. Automated GTS centers will handle seismic data within a few minutes, but manually operated centers will take a longer time for** relaying the data from other centers to the MTC centers. The relay time cannot **be accurately estimated due to the various procedures employed by each particular center. Therefore, in such cases the term 'relay time' is mentioned together with the transmission time in the table.**

4. For the purpose of this study, the WMCs Moscow and Washington were taken **to be international seismic data centers; therefore, all available seismic data will have to be transmitted to these two WlCs. The routing plan on the MTC has been developed, taking into account the available high-speed MTC segments. In the table, the total volume of data inserted by the MTC center concerned** is indicated together with the transmission time for a particular MTC center **to the adjacent I4TC centers. The total volume of data contains the accumulated volume which is transmitted from the upper-stream MTC center,**

5* As seen from the table, difficulties are foreseen in transmitting seismic data over certain GTS circuits operating with the modulation rate 50 or 75 bauds, in particular relaying of seismic data from one center to another will cause considerable handling time at certain manually operated centers. These problem areas could be summarized as follows:

- **(a) Western and southern parts of Region I (Africa), e.g. Central African** Empire, Ivory Coast, Ethiopia, Kenya and Southern Rhodesia;
- (b) South-western part of Region II (Asia), e.g. Afghanistan and Iran;
- (c) Some parts of Region['] III (South America);
- **(d) Some parts of Region** *Y* **(South-wegt Pacific), e.g. New Zealand and Indonesia.**

 $\ddot{}$

Transmission of Level 1 data through the WMO/GTS
List of seismic stations, countries, possible routing through WMO/GTS
and high speed center in the Main Trunk Circuit

Wien, Roma, Zurich, Budapest, Tashkent, Novosibirsk, Khabarovsk, Helsinki, Tokyo, Peking, Hongkong, Melbourne, New Helhi, Montreal/Toronto, Oran.

 $\ddot{}$

Table A4.2.2

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Estimated transmission time of seismic data from each centre of

Table, p. 3

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АРРЕШ31Х 4.5

Present state of the Global Telecommunication System (GTS) of the World Meteorological Organization (VJMO)

The current state of the main trunk circuits of the GTS is shown in Figure A4.3.1. The number of characters that can be transmitted on different speed circuits is shown in Table A4.3.1.

 $\ddot{}$

Number of characters transmitted on different speed circuits

 $\frac{1}{2}$

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APPENDICES TO CHAPTER 5

APPENDIX 5.1

International Data Post List of co-operating countries (February 1979)

* Listed in Table 4.1 of seismograph stations, CCD/558. ⁺Tokyo and Osaka only.

Notes;

1, Type of service ; International Datapost offers two kinds of service for business mail (which covers magnetic data tape); these are 'Scheduled' (S) or *Qn-Demand' (d).

The Scheduled service operates for regular, repetitive requirements on **' given dates and days and usually includes door-to-door collection and . delivery in the collaborating countries. The On-Demand service caters for non-regular requirements; collection and delivery services are not usually provided and users hand in or collect items from nominated postal centers in each country.**

2. Transit time ; 1-3 days, depending on distances, etc., but next-day delivery is normal between major centers. As an example of a longer distance route over which seismological data is routinely sent, magnetic tapes posted in Brasilia on Monday evenings are delivered in Edinburg, Scotland, on Thursday morning.

АРРЕШ)1Х 5-2

Calibration data to be included with exchanged waveforms

All exchanged waveforms should in general be supplemented with sufficient information so that no misunderstanding can arise with respect to station **identity, type of data', sampling rate, time and amplitude scale and time** interval covered. The following calibration information should be transmitted **with' the waveform data.,**

1. For seismographs with analog galvanometric recording

- **(a) Dimensionless magnification (displacement sensitivy) defined as the ratio of bhe peak trace amplitude to the peak amplitude digplacement of sinusoidal ground motion at a specified** frequency. The frequency will typically be 1 Hz for short period instruments and 0.05 Hz for long period instruments.
- **(^) Phase difference in seconds between peak trace amplitude and the corresponding peak ground displacement for the steady-state motion.**
- **(c) Time corrections relative to UTC at the beginning and end of the seismograra»**
- **(d) Direction of the trace deflection corresponding to ground movement in the direction up (cn the vertical component) and to the north or east (on the corresponding horiiontal component) should be ma.rked directly on the seismogram.**
- **2• For digital waveform records**
	- **(З') Quantization factor (nanometers/digital unit), i.e. the ground displacement (at a specified frequency) corresponding to 1 digital unit.**
	- **(^) Phase difference (in seconds) as under 1.**
	- **(c) Time correction (relative to UTC) for the beginning of the record.**
	- **(d) Polarity of the data (positive polarity means that the ground** movement directions up, porth and east correspond to positive **numbers on the digital records).**

Note:

Additional calibration information will be retained at each station and at **the International Data Centers, including complete phase and amplitude response characteristics for all instruments. These files are updated regularly, as new calibration are performed, and the International Centers may request** additional calibration measurements to be made as desired. It is therefore **not considered necessary to transmit this complete calibration information with every requested waveform.**

APPENDIX 5.3

Specification of waveform recording media at some seismological stations that may be included in a global network

Table 5«5»1 contains detailed specification,of waveform recording media at most of the stations listed in Table-4»1 of CCD/558, as well as for some additional stations that may be included in a global network. Note that both the operational status and the type of equipment at these stations are **subject to change.**

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 $Window$

Table 5.3.1

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Table 5.5.1 (continued)

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Table 5.3.1 (continued)

Table 5.5.1 (continued)

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Table 5»5.1 (continued)

iiPPENDIX 5.4

Some Digital Tape Recording *Standards*

The description 'Industry compatible tape' is commonly used. It means that data may be interchanged between computer systems of different manufacture as long as the tape used is to the same compatible standard. The standards for magnetic tape laid down by bodies such as European Computer Manufacturers Association (ECFA) and American National Standards Institute (ANSI) define the physical properties of tape such as spool dimensions, tape width and **thickness, recording node and density and positioning of reflective strips.** They do not define tape codes or label and block formats. Two versions of digital tape in common use arc:

9-track, 0.5 in width, 800 bits per inch (bpi) with non-return-to-zero inverted recording mode (NRZl), and

9-track, 0.5 in width, 1600 bpi with phase encoding recording node (PE). **Standards for 7-track tapes also exist (for example, the high gain long period** stations at Kipapa and Ogdensburg) but it is superseded by the 9-track standard **and is not recommended.**

Not all systems use the sane tape code, but the most common ways of recording characters on digital tape are the IBM extended binary coded decimal interchange code (EBCDIC) or the American National Standard Code for Information Interchange (ASCII). Conversion routines convert one tape code to another.

The digital labelling of tapes is dependent on the file structure arrangements of the systems which handle them. Tapes may therefore be labelled according to some convention (e.g. IBM standard) or in some non-standard way, depending upon **the requirements of a particular system.**

Tapes which are used in applications not requiring a file-structured system **(e.g. field data tapes) can be unlabelled.**

The block format of the data recorded on digita.l tape is governed by the software of the recording system; reading the tape therefore requires **appropriate softwaxe in the replaying system. Inter-block gaps on** 8**OO/**16**OO bpi nine-track tapes axe nominally 0.6 in, block lengths are dependent on recording** software parameters.

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APPENDICES TO CHAPTER 6

APPENDICES TO CHAPTER ^

Introduction

These appendices should he considered as guidelines for the further detailed specification that has to be made of the procedures to be used at international data centers.

These detailed specifications necessary for the establishment of the. international data centers should be worked out on the basis of the guidelines **given in this report, past experience at existing data centers and ideas and** results that might be obtained from studies performed in connection with the possible further work of the Ad Hoc group.

The specifications shovild include all necessary mathematical formulas and data handling routines and listings of the computer programs to be used. Travel time curves should be specified in .detail, showing for example to which region and which signal frequency they apply, also the various amplitude distance corrections to be used in magnitude calculations should be explicity given.

One of the appendices, Appendix 6.5, has been drafted to a high degree of detail to show, as an example, what such specifications might finally look like.

APPENDIX 6.1

Procedure for the association of short period Level 1 data for event definition and procedure for 3-dimensional event location

The automatic association of arrival times is the first important step in the event definition and location procedure. The association procedure involves a preliminary selection of those arrival times that appear to he associated with the same event. The sorting procedure is based primarily on teleseisraio P-wave arrival times and preliminary locations obtained from array station data. The P-wave arrival times are associated either using a preliminary array location or using .other P-wave .arrival times occurring within a given time window. '.This time window is estimated from the Jeffreys-Bullen travel time model and depends on the geographical distribution of the reporting stations Reported quantitative remarks such as "local" or "regional" are useful in this **process. Also P and S readings reported from stations at local distances may ,be used provided local travel time curves are available.**

The time association should be carried out according to a procedure which will need to he described explicitly and in detail. Certain time requirements should be specified for the acceptance of a group of associated phases as an event. Requirements should also be specified for the acceptance of the association of an individual station with an event.

A minimum number of stations are required to define an event as follows:

- Four single stations, not more than two of which are local stations
- **One array station at teleseismic distance and two single stations (with no distance restriction)**
- **Two array stations at teleseismic distances**

To further reduce the probability of malcing a wrong time association and thus create an artificial event from arrival times which happened to fit together, a special control procedure should be employed. This procedure should check that **the stations which have defined an event also have a defined — reasonable** probability of detecting an event with the actual magnitude at the actual distances, **based on a priori information on the detection capability of the stations. It should also be checked that the stations which have not reported an event do not have a high probability of detecting an event with the actual magnitude in the actual**

region. A possible event should e.g. be declared as artificial and excluded if a certain number of stations with high detection probabilities did in fact **not detect the event. A detailed description of this association control procedure will need to be worked out.**

The final locations of the events should be carried out using a 3-dimensional location procedure similar to those used at existing seismological **data centers.', A detailed description of the location procedure including an estimate of the uncertainties in the estimated source parameters should be elabçrated. The location procedure should allow for the use of data from local stations when 'appropriate local travel time curves are available.**

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АРРЕЮ1Х 6.2

Local travel time curves and the regions and distance intervals in which they are applicable

To use stations at local distances from an event for the definition and location of the event, local travel time curves are needed. These curves should be tied to individual stations or group of stations and be defined in a certain distance interval. The travel times should be given as tables or as explicit expressions.

Examples of such local travel times are given below. Region: Scandinavia lat. 55° - 70°N, long. 10° - 30°E. **Station ; Hagfors (HPS) Phase** Travel time (s) Distance interval (km) **P**_g $-0.3 + 0.167$ d $115 - 490$ **P^** 8.5 **-**1**-** 0.121 **d** 235 **-** 1250 S_g -1.2 + 0.283 d 115 - 1400 **S^** 13.0 **+** 0,213 **d** 350 **-** 1360

d denotes distance (km) between source and receiver. The travel times refer to surface foci events.

APPEND IX 6.3

Amplitude distance correction for the estimation of body wave magnitude m_p

Body wave magnitude (m_h) should be computed using the formula m_h = log $A/f + f(\Delta)$

where A is zero-to-peak amplitude in nanometers, T is period in second and $f(\Delta)$ **is a distance correction function. The Gutenberg and Richter (1956) amplitude**distance correction function should be used for distances (\triangle) greater than **20 degrees. This function is shown for the PV wave in the particular case of shallow foci in Figure A**6**.**5**.I.**

At distances below 20 degrees, further studies need to be carried out, and existing regional magnitude scales (e.g. see references below) should be studied as part of this effort.

References

Gutenberg, B., and O.P. Richter, 1956: Magnitude and energy of earthquakes. Ann. Geofisica, 9, I-I5**.**

A survey of practice in determining magnitude of near earthquakes : Summary report for networks in North, Central and South America compiled by У.Н.К. Lee and R.J. Wetmiller, United States Geological Survey, Open-File Report 76-677, 1976.

Part 2: Europa, Asia, Africa, Australasia, the Pacific, **compiled by R.U. Adams, World Data Center A for Solid Earth Geophysics, Report SE-8, 1977***

APPENDIX 6.4 **Calculation of magnitude**

The discussion below is limited to the estimation of surface wa**v**e magnitude M_s, but the formulas and procedures are equally applicable to body wave magnitudes, m_i .

The most common way of calculating the magnitude of a seismic event is based on straight forward averaging. From the reported zero-to-peak amplitude (a) in nanometers and period (t) in seconds individual station magnitudes, calculated according to the formula;

 $M_{\rm ej} = \log (A/T)_{\rm i} + 1.66 \log (A/\rm i)_{\rm i} + 0.3$ **where i denotes station index running from 1 to the total number of stations (N) having** \bullet **3** \bullet **10** \bullet **standard deviation is also calculated as a measure of the data scatter. Values significantly deviating from the mean, e.g. by more than three times the standard deviation are sometimes discarded.**

From a statistical point of view mean values formed in this way can be strongly biased. This could occur in particular for weak events with only a small number of **observations of (a/t). In such cases this [type of](file:///ieak) mean values become too large.** Maximum likelihood methods, which reduce the bias, have been suggested by **Mngdal (**1976**), Elvers (I**978**), von Seggern and Rivers (197S) and Ringdal (**1978**). These methods, which assume that observed station magnitudes are subject to normal distributions, combine reported amplitude period ratios with noise values at stations where no signals have been detected. It can be noted that noise amplitudes are included in the list of Level 1 data to be reported (Cf Chapter 3)* An appropriate maximum likelihood method to be used for magnitude estimation at international data centers can therefore be specified. Methods have also to be developed that give estimates of upperbound surface wave magnitudes for events, for** which body waves but not surface waves have been detected (Elvers, 1974). **Specifications for making such upperbound estimates should also be given further study.**

References Ringdal, F, 1976 Maximum likelihood estimations of a seismic magnitude. Bull. Seism. Soc. Am., 66:789-802. Elvers, E, 1978 Seicnic magnitude estimates, with a minimum number of detections, FOA report April C 20234-T1. National Defense Research Institute, Stockholm. Elvers, E, 1974 Seismic event identification by negative evidence. Bull. Seism. Soc. Am., 64:1671-1684. Von Seggern, D and Rivers, D.W, 1978 Comments on the use of truncated distribution theory for improved magnitude estimation. Bull. Seism. Soc. Am., 68:1543-1546. Ringdal, F, 1978 A reply to "Comments on the use of truncated distribution theory for improved estimation" by von Seggern and Rivers. Bull. Seism. Soc. Am., 68:1547-1548.

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APPEND EC *6.5*

Travel times for Rayleigh- and Love-yaves for continental and oceanic structures

This appendix has been drafted to a high degree of detail to show, as an **example, what the specifications of the procedures at international data centers might look like.**

The appendix gives initially a brief description of the mathematical formulas used.

Table A6.5.1 gives the Rayleigh-yave group velocity (after Filson, 1974) for **continental and oceanic structure to be used for estimating the arrival times of Rayleigh-waves at individual stations from events located from short period data.**

The map shows in 5° x 5° areas the regions to which the two structures should be **applied.**

A listing of a computer program for the computation of Rayleigh-wave travel times **from an epicenter to a recording station is given in subappendix 5A.**

Data for Love-waves are not included in this example, but similar tables should he worked out for this typo of \/ave.

Reference

Filson, J.R., 1974 **Long period results from the International Seismic Month.** Lincoln Laboratory Report 1974-15, Massachusetts, USA. **Procedure for calculating surface-wave travel times**

The surface *i.aves are assumed to follow great circle paths from source to* **receiver (distance D). The distance D is divided into parts belonging to regions with different group velocity curves. Thio is made by a step procedure.**

In the figure the line PQ denotes a great circle path between source and **receiver. As is shovm in the figure p and a are colatitude and longitude of P and с and b colatitude and longitude of Q. U is the north pole. A point M is moved from P to Q by increasing d in small steps. For each step the colatitude (m) and the** longitude (a+n) of M are calculated. The following formula is used for **calculating m:**

cos m = cos d . cos p + sin d sin p cos az

This is obtained from the spherical triangle PMM, where az is the azimuth to **Q vievred from P (d, p and az are knovm). The same formula applied again to РИМ gives n ;**

 $\cos d = \cos p \cos m + \sin p \cos m \cdot \cos n$

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The correct solution of n (positive or negative value) is chosen depending on **if az is greater than or less than 180".**

To avoid nximerical problems care is talcen to cases v/hen P, Q or M are close to one of the poles or when D is close to 130°.

The earth is divioed in a grid *\iith* **r (longitude) times s (latitude) number of squares. The grid spacing is several times the increment of d. A matrix corresponding to the grid indicates \/hich region each square in the grid belongs to. By transforming the coordinates of II to matrix indices**

index $1 = \frac{a+n}{360}$. **r** + 1; **index** $2 = \frac{m}{180}$. **s** + 1

the region in which M is situated is found. By summing up the number of steps taken in each region the distance D is divided into parts belonging **to the various regions. The travel time is, then calculated as the sum of the travel timeé within the different regiops as follows;**

$$
{}^{T}t = \frac{D}{r} \sum_{i=1}^{k} v_{i,t}
$$

\n
$$
k_{i} =
$$
 number of steps in region i
\n
$$
v_{i,t} =
$$
 group velocity in region i for waves with period t
\n
$$
{}^{T}t =
$$
 travel time from source to receiver for waves with period t

Table A6.5.1

Period	Group velocity $(\text{km/s})^2$			
(\sec)	Region 1 (Ocean)	Region 2 (Continent)		
1	1.95	1.00		
\overline{c}	1.70	1.20		
3	1.45	1.50		
4	1.20	1.70		
5	1.05	2.00		
6	1.00	2.50		
$\overline{7}$	0.98	2.70		
8	1.00	3.00		
9	1.02	3.15		
ıò	1.10	3.15		
11	1.15	3.15		
12	1.25	3.15		
13	1.35	3.10		
14	1.60	3.10		
15	1.80	3.10		
16	2.20	3.05		
17	2.65	3.00		
18	2.95	2.95		
19	3.25	2.95		
20	3.40	2.95		
21	3.60	2.95		
22	3.70	2.95		
23	3.75	3.00		
24	3.30	3.80		
25	3.85	3.05		
26	3.85	3.05		
27	3.90	3.10		
28	3.90	3.15		
29	3.90	3.20		
30	3.90	3.25		
31	3.90	3.30		
32	3.95	3.35		

Period	Group velocity (km/s)		
(\sec)	Region 1 $(0$ cecn $)$	Region 2 (Continent)	
33	3.95	3.40	
34	3.95	3.45	
35	3.95	3.45	
36	3.95	3.50	
37	3.95	3.55	
38	3.95	3.60	
39	4.00	3.60	
40	4.00	3.65	
41	4.00	3.65	
42	4.00	3.65	
43	4.00	3.70	
44	4.00	3.70	
45	4.00	3.70	
46	4.00	3.75	
47	4.00	3.75	
48	4.00	3.75	

Table A6.5.1 (cont.)

Subappendix A5 0.310 SUBROUTINE TITME(COLAE, CLONE, AZS, DIST, TIM, PI, NL, IGV) $0.120C$ **JOUSJ C+** INGVAR JEPPSSON, LOA 202, 790109 $00040 C$ 06/050 C $00000C*$ THIS ROUTINE CALCULATES THE TRAVELTIMES FOR SURFACE WAVES FPOM AN COOTO C EVENI TO A SEISMIC SIATION. IRAVELTIMES ARE CALCULATED FOR UP TO FOUR DIFFERENT SURFACE WAVE OGGPO C (7) , 90 C PERIODS. $C.1100C$ 00110 C THE EAPTH IS DIVIDED IN A NUMBER OF REGIONS, EACH REGION IS GIVEN (X) 120 C A NUMBER. TO EACH REGION BELONGS A GROUP VELOCITY CURVE WITH THE 00130 C SAME NUMBER AS THE REGION (THE GROUP VELOCITY GIVEN FOP PERIODS OG 1.35 C RETWEEN 1 AMD 48 SECONDS). 00130 C THE EARTH IS ALSO DIVIDED IN A GPID, AND TO THIS GRID COPPESPONDS 0.0150 C A MAIRIX. FACH ELEMENT IN THE MATRIX CONTAINS A NUMBER FOUAL TO $9.161C$ 00170 C HIE NUMBER OF THE REGION THE CORPESPONDING SOUARE BELONGS 10. $00150C$ $(0)190C$ THE TRAVELTIME IS CALCULATED AS THE TRAVELTIMES WITHIN 0J200 C EACH REGION. SO. FIRST THE DISTANCE THE SURFACE WAVES IRAVEL WITHIN 00210 C EACH REGION IS CALCULATED, ASSUMING THE WAVE TRAIN TRAVELS ALONG A 0.0220 C GREAT CIPCLE PATH (NO REFPACTION OR MULTIPATHING). THIS IS MADE BY $(D230)$ C A SIEP PROCEDURE FROM EVENT TO STATION. THE NUMBER OF STEPS TAKEN IS 00240 C SUMMED UP FOR FACH REGION AND THE NUMBER OF STEPS IS THEN CONVERTED $00250C$ 10 DISTANCE. $0.260C$ $(0.270C)$ CODED C EOIAIION: 00290-C ALL ANGLES IS GIVEN IN RADIANS IF MOTHING ELSE IS STATED. $0.13C0C$ COLAF, CLONF = COLAIITUDE AND LONGITUDE OF THE EVENT $00310C$ $0.320C$ COLA=COLAE. CLON=CLONF 00330 C AZS, DIST = AZIMUTH AND DISTANCE FPOM EVENT TO STATION 00.340 C Λ 7 = Λ ZS 00350 C $11M(J)$ = TRAVEL TIME FOR SURFACE WAVE WITH PERIOD PT(J) 00.360 C $PT(J) = SURFACE$ WAVE PERIOD (J=1 TO NL) 00370 C NL = NUMBER OF PEPIODS FOR WHICH TPAVELTIMES SHALL BE CALCULATED $003 \rightarrow C$ (NUMBER OF PERIOD MEASUPEMENTS: MAX 4) IGV = PARAMETER DENOTING TYPE OF WAVE PATH USED AT MAGNITUDE DETERMINATION (IGV=1: MORE THAN 75% OCEANIC STRUCTURE: $00290C$ C^*) \wedge C \vee C IGV=3: MORE THAN 75% COMTINENTAL STRUCTURE: IGV=2: OTHEPWISE) $12410C$ GUZGO C IPESCII, I2) = MAIPIX CONTAINING REGION NUMBERS FOR ALL SOUARES U.JA \mathcal{F}_L C IN THE CRID IIN. I2N = MAXIMUN VALUES OF I1 AND I2 RESP. (IIM+I2N=RUNBED OF (3777) C 33450 C SOUARES IN THE CRIDI (0.4ω) C GRIDG, GRIDL = IATITUDIMAL AND LOMGITUDINAL SIZE OF A SOUARE IN THE GPID (IF I1M=36 AND I2M=72 A SOUARE IS 5*5 DEGREES) 00470 C NR = TOTAL NUMBER OF REGIONS (AND GPOUP VELOCITY CUPVES) OUZRO C $CO190$ C VELR(1, T) = GROUP VELOCITY CURVES. THE MATPIX CONTAINS THE GROUP $0.900C$ VELOCITY FOR SUPEACE WAVES WITH PERIOD T IN PECION NUMBER I 00510 C (ER=MAX VALUE OF I) 00520 C $I =$ REGION NUMBER 005.30 C $T = PERTOD OF SUPERCE WAVE CINTER)$ 00540 C D = DISTANCE FROM THE FVENT TO A POINT M (IN DIRECTION AZS) 00550 C CM, LM = COLATITUDE AND LONGITUDE RESP. FOR POINT M DM = DIFFERENCE IN LONGITUDE BETWEEN THE POINT M AND THE EVENT $O(D^{\prime} O)$ C 00570 C $DP = STEP$ SIZE $00550C$ $DDC = STEP$ SIZE IN DEGREES 0.3590 C $P(1) = S1EP$ COUNTER FOR REGION I PP = TOTAL MUMBER OF SIEPS (SUM OF ALL P(I) WHEN STATION IS REACHED) 00600 C 00610 C PART(I) = DISTANCE IN REGION I OF THE SURFACE WAVE PATH W G O C COCE, COAZ, COD, COCM, CODM = COS-VALUES OF COLA, AZ, D AND DM RESP. 00630°C SICE, SIAZ, SID, SICM = SIN-VALUES OF COLA, AZ, D AND CW RESP. 00640 C $TWOPI = 2*PI$ LOGSO C DECKM = LUMBER OF KILOMETERS PER DECREE. 606.40 C IT = NUMBER OF OUTBUIL UNIT FOR ERROR MESSAGES AND WARDINGS $\omega_{\rm{c}}$ and $\omega_{\rm{c}}$

 -30650 C DECKY = NUMBER OF KILOMETERS PEP DECPEE. $00660C$ IT = MUMBER OF OUTPUT UNIT FOR EPPOR MESSAGES AND WARNINGS $0.0670C$ 00680 C ALL STATEMENTS APE STANDAPD FORTRAN EXCEPT THOSE PRECEDED BY A LINE $00690C$ BEGINNING WITH C*** 00.700 C $00/10^{\circ}$ C. REAL PART(2), P(2), LM, C'1, TIM(4), PT(4) 00720 00730 INTEGEP T (207.40) COMMON ZLP1ZIREG(36,72), VELR(2,48) (0.75) DATA IT/6/, NR/2/, DDG/1./, DEGKM/111.2/ 00760 PATA PIZ3.141593Z, IIMZ36Z, I2WZ72Z, TPOPIZ6.283186Z $00770C$ CHECK IF ANY OF THE PAPAMETERS IN THE SURROULINE CALL STATENEUT (20.76) C $C3790C$ IS OUT OF RANGE. $0.3 - 3.3$ C 20.11 IF (COLAE.LT.O..OR.COLAE.GT.PI.OR.CLONF.LI.O..OP. 00 (22) +CLOFE.GT. INOPI.OR.AZS.GT. TWOPI.OR. ∞ \approx 30 *AZS.LT.O..OP.DISI.LT.O..OP.DIST.GT.PI) GO TO 5CO $COCMO$ C $(93.4.3)$ \sim SEI COLPECI VALUES TO SOME PARAMETERS AND SET COUNTEPS TO ZEPO. 001 GO 10 Q) \leq 70 B GRIDC=PIZELOAT(IIM) $00 \div 30$ GRIDL=TWOPIZELOAI(I20) $CO₂$ (2.) $[1] = [1]G*PI/180$. $Q()$ ^{Q} Q Q $[1, 1]$ $[10, 90, 1 = 1, 19]$ 00912 $(1)920$ $Q() P(1)=0.$ $(Y) \subseteq \{t\}$ COLA=COLAE 00.940 CLON=CLONF 00 950 $A / = A / S$ 009 on C SIVE AZ A WELL DEFINED VALUE IF DIST IS CLOSE TO 180 DEGPEES. 00970 C 00989 C 00970 IF $(DIST, GT, (PI-0, 001))$ $N^2=0.1$ 01000.0 CHECK IF THE EVENT IS CLOSE TO OME OF THE POLES. 01010 C $01320C$ IF (COLA.LT.0.001.0B.COLA.0I.(PI-0.001)) GO TO 650 01933 $UL40C$ $01050C$ CALCULATE FPEOUENTLY USED SIN- AMD COS-VALUES. 01060 C 01070 100 COCF=COS(COLA) 01.30 $SICF = SIM(COLL)$ 01090 $COAZ=COS(AZ)$ 01100 SI $Y=SI$ $N(\Lambda Z)$ 01110 CM=COLA 01120 LM=CLON CO TO 400 01130 01110 C $01150C$ INCREASE DISTANCE D FROM EVENT TO POINT M WITH STEP DD. 01160 C 01170 $150 + 1=11 + 11$ 01130 C WAS THE STATION PEACHED WITH THIS STEP? $01190C$ 01200 C 01210 IF (D.GT.DIST) CO IO 1000 01220 C 01230 C 01240 C $01250C$ CALCULATE THE COOPDIDATES (CM, IM) FOR POINT ". 01260 C 01270 $CO(D=CO(5(1))$ 0120 $G11 = G111(f)$ 01250 CO 25400 NHCO DECEMBER SEL HOOM!

 $J1 < I$ $(39) = (305(1))$ 31250 $SID = SIN(1)$ 012.01 COCM=COCE*COD+SICE*SID*COAZ $013C₂$ C $[11, 21]$ \cup CHECK HI ARCCOG-ARGUMENT IS OUT OF PANCE. $01320C$ 01.300 IF (APS(COCM).GT.1.0) GO TO 710 $01340C$ ** 21.350 340 CM=APCOS(COCM) 01360 C 01270 C CHECK IF M IS CLOSE 10 ONE OF IPE POLES. 01.380 C 01390 IF (CM.I.LO.0001.OR.CM.GT.(PI-0.0001)) GO 10 720 31400 $SICM = SIM(CM)$ 01410 $COMM = (COMP-COCExCOCM)/ (SICExSICM)$ $01420C$ 01.430 C CHECK IF ARCCOS-ARGUMENT IS OUT OF RANGE. 01740 C H^*M IF (ABS(CODM).GT.1.0) CO 10 739 $01460C +$ * 01470 350 DM=ARCOS(CODM) $014P)$ C 014.20 C CHOSE THE RIGHT SOLUTION OF DM DEPENDING ON AZIMUTH. $H^{E}(A)$ C $Q1 + P$ 360 IF(AZ.GT.PI) DM=-DW $H₁$ $C₂$ $015 - 0$ CALCULATE LONGITUDE OF POINT M AND CHOSE RIGHT INTERVAL. $O1² \rightarrow C$ $O(4410)$ $I M = CI ON + DM$ $\gamma_1 \cdots$ IF (LM.LT.O.) LN=LM+1WOPI as N IF CLM.SI.TWOPI) LM=LM-TWOPI $015.20 C$ OFFINO C $O1600^\circ C$ $01610C$ CALCULATE WHICH SOUAPE THE POINT M (WITH COORDINATES CM, LM) (11620) C FALLS WITHIN: THAT IS DETERMINE THE VALUES OF THE INDICES 0163 $0C$ TO T'E IPFG-MATRIX AND DETERMINE WHAT REGION THE SOUARE $01630C$ BELONGS TO (REGION NUMBER=I). START WITH M = EVENT. $01650C$ INCREASE APPROPPIATE STEP COUNTER. 01650 C 400 II=IFIX(CM/GRIDC)+1 01670 $0163.$ $I2 = IFIX(LM/GPIDI) + I$ 01690 IF (FILIT.1.0P.II.CT.11M.OP.I2.LT.1.0R.I2.CT.12M) GO TO 700 $I = [PFG(11, 12)]$ $Q1/Ln$ 01711 $P(I) = P(I) + I$. 01721 CO 10 150 $01720C$ 0174 C $01750C$ 0176) C OUTPUT OF ERROR AND WARNING MESSAGES. $01770C$ 01720 500 WPITE(11,501) COLAE, CLOME, AZS, DIST 501 FORMAI(1X, <*****APHING: TTIME-ARGUMENI OUI OF PANGE:</ $01/9.$ 01ω $*1X$, \prime EVENT LAT, LONG 4, 2F8.5, 5X, りはい \star AZIMUTH, DISTANCE 4, 2F3.5) 01820 C 01630 C NO COPPECTION OF THE ARGUMENTS IS MADE. $01830C$ 01850 GO TO 85 $O1860C$ $01870C$ 01889 650 WRITE(IT, 651) COLA 01890 651 FORMATCIX, ZEERVENT CLOSE TO OME OF THE POLES: COLAI=Z, FO.5) 01900 C $01910C$ MAY CAUSE FUNERICAL TROUBLE. SEI TEN VALUE. $01920C$ 01939 IF $COLA$.LT.0.(01) $COLA=C0.1$ 01939 $HECOI, V, C1, (PI-C, 001)$ $CV := PI - .$ 司机 机工 $30 - 100$

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IF(COLA:GT:(PI-0.001)) COLA=PI-0.001 01277 0.104 **CO TO 100** $O(S \land Y)$ C ||G1|||711|||C 31930 700 SPIECIT, 701) 11, 12 $O(1.03)$ 701 LORMA LCTX, P*** LREGEARMUNENT OUT OF PANGE® T1=2, 13, P = 12=2, 13) $Q2CC$) C $J2010C$ IF IREG-ARCUMENT IS OUT OF BANGE THIS STEP IS IGNORED (NO STEP C20.20 C COUNTER INCPEASED). 02.30 C $(12, 4)$ CO TU 150 02₀50 C 020.60 C 02070 710 IF (ABS(COCM).LT.1.001) GO TO 715 02U.20 C 02090 C NO MESSAGE IF OMLY TRUNCATION EFROR. 02100 C 02110 SPITE(IT. 711) COCS 02120 711 FORMICIX, Z***ARCCOS-APGUMENT OUT OF RANGE: COOM=2, F12.8) 021.35 C IF ARCCOS-APCUMENT IS OUT OF RANGE, IT IS COPPECIED TO +1, OP -1. $021477C$ PESPECTIVELY PUDEPENDENT OF THE ACTUAL VALUE. AND THE EXECUTION 02150 C $0.216.2C$ IS COMINUED. $0217.7 C$ 715 COC-=SIGN(1., COCD) $Q21(4)$ 021 70 CO TO 340 022CO C $02210C$ 02220 720 WRIIF(IT, 721) CM 721 FORMATCIX, K***M MEAR ONE OF THE POLES: COLAIN=4, F12,8) (223) 02240 C 02250 C GIVE DM A WELL DEFINED VALUE. 02250 C 02270 $IM=O$. $022 - 0$ CO TO 360 02290 C $023(1)$ C 02310 730 IF (ABS(COM). [T.1.001) 00 TO 735 $02320 C$ NO MESSAGE IF ONLY TRUNCATION EPROP. 02330 C $(1234.)$ C 02350 WRITECIT, 731) COM 731 FORMATCIX, <***ARCCOS-ARGUMENT OUT OF BAFGE: COM<, F12.8) 02360 $0.2373C$ TE APCCOS-ARGUMENT IS OUT OF RANGE, IT IS COPPECTED IO +1, OP -1. $O(2.35)$ C RESPECTIVELY INDEPENDENT OF THE ACTUAL VALUE, AND THE EXECUTION 02399 C $Q24(k)$ C IS CONTINUED. $02410C$ 735 COM=SIGN(1., COM) (PA) 024.00 GO TO 350 $0244) C$ $024 - 0 C$ 024 o0 C 02470 C CALCULATE THE DISTANCE IN DIFFERENT REGIONS OF THE WAVE PATH. 02430 C FIRSI. SUM UP THE TOTAL MUMBER OF STEPS. 02490 C 02500 COO PP=0. 02510 $[10 \ 1001 \ 1=1$, MR $0,25,20$ $CO1$ PP=PP+P(I) 02530 $[10, 1005, I=1, MR]$ $02 - 10$ 005 PART(I)=P(I)*DIST/PP $021.50C$ 02560 C $0.470C$ 02599 C* CALCULATE THE TRAMELTIME AS THE SUM OF THE TRAVELTIMES IM THE 02590 C PIFFERENT REGIONS, AND MULTIPLY BY A CONSIALL FACIOR TO CEL THE 0260J C IPE P SECONDS. 02610 C $\Omega^2 \to Y$ $\left\langle \mathbf{P}\mathbf{P}^{\prime}\right\rangle \left\langle \mathbf{I}\right|\mathbf{I}\left\langle \mathbf{Y}\right\rangle \leq\left\langle \mathbf{I}\mathbf{m}^{\dagger}\mathbf{I}\right\rangle _{0}\leq\mathcal{I}$

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ON REPORT REGIONS, AND MULTIPLY BY A CONSTANT PACTOR TO SET THE T $0260 + C$ INFIN SECONDS. $02612C$ $E0$ 1100 J=1, 4 (22620) 0263) 1100 11:101=0. $100 - 1155$ J=1, M 0263) (1265) $I = ITIX(PI(1)+0.5)$ DO-1459 1=1; PP 0266.7 02675 1150 TIM(J)=TIM(J)+PART(I)/VFLR(I, I) 02690 $TIW(J)=TIM(J)*DECKM*130.7P1$ 02690 1155 CONTINUE $Q27CQ$ C 02/10 C 02720 C* CONVERT TO TENTH OF SECONDS BY MULTIPLYING BY TEM. 02730 C 0274.1 DO 1160 J=1. NL $02750 - 1160$ TIA(J)=TIM(J)*10. 02750 C \sim \times ℓ $\sim c$ \mathcal{L}^{max} JZ $C+$ CALCULATE VALUE OF IGV DEPENDING ON WAVE PATH. $0279 + C$ IGV=1 FOR HOPE PIAN 75% OCEANIC STRUCTURE $U2E(G)$ C IGV=3 FOR WORL THAN 75% CONTIMENTAL STRUCTURE $[028116]$ IGV=2 OTHEPWISH $02.50C$ $\frac{0.256388}{0.252833}$ SPAPI=PART(1)ZDIST $ICV=2$ $(22, 4, 3)$ 1F (SPAPI.GI.0.75) [SV=1 021.61 IF $(CPAR1.LT.0.25)$ $IOV=3$ $02 - 7.1$ C $(02²)/C$ $\sim 10^{-1}$ **FriUPH** \sim רפעס 上出厂

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APPENDIX 6.6

Automatic process for the association of long-period **surface wave data with events located from short-period observations**

A procedure by which reported long-period surface wave data are associated **with events located from short-period data shovild be used at international data centers.**

The travel times for long-period Rcyleigh and Love waves from an epicenter to the long-period stations arc estimated using the travel times given in Appendix 6**.**5 **. Reported long-period surface wave data should he preliminary** associated with an event if the estimated arrival times of surface waves at **a certain period agree with those reported within a predetermined time interval.** To reduce the probability of making a wrong association of surface waves, a **procedure similar to that discussed for short-period signals in Appendix 6.1 could be applied. This procedure checks that stations to which surface waves** have been associated also have a reasonable probability of detecting such signals **from an event with the actual magnitude at the actual region. A detailed description of the association control procedure will need to be elaborated.**

APPENDIX 6.7

Example of output bulletin and data file structures at Internatio al Data Centers

Example of a possible format of an output bulletin (containing basic $1.$ information) from an International Data Center for one event

780120 $0.02421.6 \pm 7.3$ 9.6s \pm 0.1 159.3E \pm 0.1 28 km \pm 10 BASED ON 12 STAT SOLOMON ISLANDS NUMBER OF ASSOC. SP-TIMES 34 NUMBER OF ASSOC. LP-TIMES 8 MB : 5.1 BASED ON 6 STAT STD : 0.30 $MS \rightarrow :$ 5.0 BASED ON 7 STAT STD : 0.35 CMPX : 1.23 SPMM : 1.21 SPVT : 0 -9 -18 -13 -37 STAT : ARR. Explanations $780120 = date of event$ 002421.6^{\pm}7.3 9.6S \pm 0.1 159.3E \pm 0.1 28 km \pm 10 BASED ON 12 STAT = origin time, epicenter, depth with associated error estimates and number of stations used for defining event SOLCMON ISLANDS = $region$ NUMBER OF ASSOC. SP-TIMES 34 NUMBER OF ASSOC. LP-TIMES 8 = number of short period and long period arrival times that could be associated with the event MB : 5.1 BASED ON 6 STAT STD : 0.30 = estimated bodywave magnitude based on amplitude and period measurements at 6 stations. Standard deviation among the individual station magnitudes is also given. MS : 5.0 BASED ON 7 STAT STD : 0.35 = estimated surface wave magnitude based on amplitude and period measurement . at 7 stations. Standard deviation among the individual station magnitudes is also given. CMPX: 1.23 SPMM: 1.21 SPVT: 0 -9 -18 -13 -37 STAT: ARR.

= identification data for the event as reported from station ARR.

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2. Bata file formats

The data storage at-the data centers could preferably be divided into several data files as follows:

- **Station parameters and calibration data**
- **Input data, reported from individual stations**
- **Output parameters obtained as a result of the processing at the centers**
- **Internal "book-keeping" files**
- **Level 2 data files.**

These data files should be identical at the different data centers and they should be arranged so that data are easily accessible by modern computer **techniques. Detailed specifications of the format used for the various data files will need to be elaborated. An example of a possible structure-of data files at international'data centers'is given at the end of this appendix.**

Station parameters and calibration data file

This file contains station parameters such as latitude, longitude, instrument and regularly updated calibration data. This file should also contain information about the time intervals during which any individual station has been out of operation.

Input data file

The file contains all the information that has been reported to the data centers via the WMO/GTS. The contents of this file depend on what actually **are reported from the individual stations as discussed in chapters 3 and 4»**

Output data files

These files should contain the parameters obtained as a result of the data processing at the centers. They should also contain all the individual **station data that are associated with an event. The output file should furthermore contain all the unassociated data.**

Internal^{'s}book-keeping" file

This file should contain a record of the processing that has been carried out **at the individual centers. It is quite similar to the internal data files which are presently kept at large data centers.**

Level 2. data file

This file would contain all the digital Level 2 data that have heen forwarded tb the data centers as results of requests. There will alpo be a need for archival storage of Level 2 data received on non-digital form.

3. .An example of a possible structure of data files, at International Data Centers ,

In the following, an example is given of a possible structure of data files at international data centers.

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Structure and basic functions of data banks in international- centres The purpose of a data bank is ; To store all data received by the international centre from stations in the **global network; To store data processed in the centre;** To ensure the prompt supply of necessary information at the request of States **parties to a treaty on the complete and general prohibition of nuclear-weapon tests.** Figure-6,7.1 gives a schematic view of a bank's structure. The data bank's **information control system comprises the following main elements; Input and output programmes; Bank software (set of programmes);** Bank information fund; **Bank information retrieval language; Information system hardware; Information system service personnel. The information fund can be divided into four large files, according to the nature of the data stored in it:**

I. Focal parameters of events located by the centre;

II. Calibration data and particulars of stations;

III. Signal parameters (Level-1 data) from each individual station;

rv. Original recordings of P and L waves of events (Level-2 data) for each individual station;

The basic functions of a bank's information control system are as follows; To record seismic data on machine carriers (files I-IV);

To store seismic data on the machine carriers for the regulation period; To supply stored information upon request within the established time-limit and in a specially processed form,

Depending on the operational requirements of the international centre, the bank may be equipped with an automated data-control system ensuring the rapid retrieval and supply of required information.

The type of data to be stored in the bank can be seen in tables 6.7.1- 6**.**7 **.**5 **. IkbIe'é.Y.l represents file I, which stores the focal parameters of seismic events located by the centre. Clearly, the format to be used for data in file I should be the same as that used for the bulletin of seismic events, which includes 22 parameters. Parameters 1 and 2 (number and date of event) should be used for information-retrieval purposes.**

Figure 6.7.1. Example of Structure of the data bank of an international centre in the global network

Diagram 5.1

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Table 6**.**7,2 **represents file 11, which, in addition to the specifications of SP and LP instruments, gives some basic information about the stations (co-ordinates, soil conditions). Pile 11 has 11 parameters. Parameter 1 should be used for information retrieval.**

Tables 6.7.3 and 6.7.4 represent file III - Level-1 data from all stations in the global network. This file is subdivided into two: file III-A and file III-B. File 1II-A (Table 6.7.3) is designed to store data that have been associated with **located events; file lll-B(Pable** 6**,**7 **.**4 **) is designed to store "isolated signals", which, after appropriate processing in the centre, cannot be associated with a located focus. Each of the two files is in turn subdivided into M subfiles (M = пгипЬег of stations). Each subfile in file 111-A contains Level-1 information for each consecutive located event. Only the first five parameters are standard, and the remaining data can be sent from stations in telegraphic form. The volume of data sent in this manner will differ according to the nature of the signal recording. Paxameters 1 and 2 can be used for information retrieval.**

Each of the 111-B subfiles stores Level-1 data related to "isolated" signals detected at a given station. In this case, the first three parameters are standard for all signals and may be used for information retrieval purposes. The texts of telegraphic communications from a given station could be stored with Level-1 parameters.

Table 6.7.5 represents file IV in station No.1. It contains segments of signals **recorded on SP and LP instruments. The bank could store, for a set period, 60-second segments of P waves, 30 seconds of noise from SP vertical instruments, 20-minute segments of L waves from three-component LP instruments and 5 minutes of noise from vertical LP instruments. Pile IV is subdivided into M subfiles (M = number of stations). Each subfile stores information on each consecutive event in connexion with which one or another State has requested information from a station in the global network. Each event in the subfile is defined by 6 parameters, with parameters 1 and 2 being used for information-retrieval purposes.**

Input and output programmes serve to enter into the bank Level-1 and Level-2 information and focal parameters obtained as a result of processing by the centre and to retrieve listed data when a request is submitted. Level-1 information and data from the catalogue of events should be transferred from the centre in the form of digital files. It is probable that, initially, at least for some of the stations, it will be in photocopy form only that Level-2 information can be transmitted to and from the centre.

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${\bf Table}$ 6,7.1 **P i l e I (focal perauieterc)**

 $\frac{1}{2}$

 $\mathcal{L}^{\text{max}}_{\text{max}}$, $\mathcal{L}^{\text{max}}_{\text{max}}$

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TabD-e 6-7.2 File II (sta.tion parameters)

No. of parameter	Type of station parameter	Unit of measurement	Accuracy of measurement	Volume of data $\frac{1}{2}$ words 16-bits)
	Number of the station			
\overline{c}	Station latitude	dogree	0.01	
3	Station longitude	degree	0.01	
4	Type of bedrock			
5	Height above sea-lovel	metre		
6 7	SP instrument frequency res- ponse: Z -component $(0.25 - 10$ Hz) NS-component ($\mathbf{1}$	$nm-Hz$ $nm-Hz$		30 30
8	EW -component $($ " $\pmb{\mathcal{H}}$	$nm-Hz$		30
9 10	LP instrument frequency res- ponse: Z -component $(1 - 100 \text{ secs})$ NS-component	$nm-Hz$ $nm-Hz$		40 40
11	EW-component	$nm-Hz$		40
12 [°]	Dete of last determination of instrument specifications			

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No. of parameter	Type of signal parameter $(Lorel-1)$	Unit of measurement	Accuracy of neasurement	Volume of data (com- puter words -16 bits
	Fumber of event $(Mo. 1)$			
\overline{c}	Date of event	year, day, month		
$\overline{3}$	Epicentre azimuth	degree	0.1	
4	Epicentral distance	degree	0.1	
5	Local station correction		J.	
	for travel time of P-wave	second	0.1	٦.
6	Focal correction for P -wave	second	0.1	ı
	Text of telegraphic message from station No.1 concer- ning event No.1 as detected on SP and LP instruments $(Level-1$ parameters) $SEISIO$ STOP			
	Number of event $(No. X)$			
Q.	SEISHO STOP			

Table 6.7.3

File III-A-I (Station No. 1, identified signals from located events)

<u>Table 6.7.4</u>

File Ill-B-I (station No. 1, signals not identified with located events)

 \mathbb{Z}^2

Pile IV-I (Level-2 data at Station No. l)

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The bank software would consist of a set of information-fund control programmes and an information retrieval service. Data received for storage in **the bank need not be subject to any additional processing or conversion. Thus,** the bank software could be confined to data control and retrieval programmes.

The bank information retrieval language is the form in which seismic data **arc printed out. It must be based on parameters selected to suit each file in** the information fund. The parameters selected for information-retrieval purposes play a particularly important role in the bank data-control process.

У Р Д Ю 1Х 6.8

Estination of Level 1 and Level 2 data vclunes to be handled ab International Data Centers

This appendix contains an estimate of the Level I and Level II data to be received and processed at the centers. The purpose of this estimate is to form a basis for a specification of the equipment needed at the international centers. **Note that the estimates of data volumes at Level I given in this appendix are not** directly comparable to those specified in Appendix 4.2 for data transmission on the WMO/GIS, since the coding procedures are entirely different.

Level I data

The structure of an international center and the organization of its work are closely linked v;ith the size of the information flow into the center, and, consequently with the volume of the information to be stored in the data bank over long periods. Rough estimates of the ilov; and the volume cf **data to be stored in** the center can be made on the basis of the number of computer words (16 bits each) **required to describe a single event on SP or LP equipment at Level I (see Tables 3*1 and 3.2). Such an estimate is given in Table Лб.8.1, for the purposes of which it was assumed that the global network will consist of** 25 **type-I stations,** 15 **type-II stations and 10 type-III stations.**

The number of events recorded by stations in the ϵ lobal network depends on a number of geophysical and other factors. The basic factors are: The level of seismic activity at the time.

The level of seismic noise normally detected by the stations.

The position of a station relatively to the high-seismic-activity zones. The sensitivity of the equipment and the manner in which it is installed in the station.

The methods used to distinguish signals from noise.

The number of signals recorded at individual stations over a 24-hour period may vary considerably from a few to 100 or more, depending on the factors listed above. The wave configuration of the signals recorded at a given station is also governed by a number of geophysical factors (magnitude, focal depth, epicentral distance, etc.). Thus, in the case of weak events at teleseisnic distances, SP instruments normally register only longitudinal wave groups. Deep-focus events are normally marked by an absence of surface waves.

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Since most of the events recorded at any given station are small in magnitude and have their focus in the earth's crust, most signals consist of trains of longitudinal waves recorded on vertical SP instrument.

For the sake of simplicity in calculating the data flow from stations to a center, it is assumed that over a 24-hour period each station records an average of 50 signals, 30 of which consist only of longitudinal waves detected on SP instruments and the remaining 20 of which consist of P and S waves detected on SP instruments and P, S and L waves detected on LP instruments.

Table A6.8.1

Volume of Level 1 data from stations to an international center over a 24-hour period

Using the data provided in Table A6.8.1, it is possible to calculate approximate over-all Level I data flow to a center from all 50 stations in the global network over a 24-hour period.

Thus, the over-all volume of data that will be received by a center over a 24-hour period anounts to: $73,750 + 44,250 + 38,300 = 156,300$ computer words.

Level IT data

The approximate volume of Level II data received by a center from stations in response to requests can be estimated on the basis of the assumption (which is of course highly uncertain) that information concerning five events characterized by P and L waves will be requested each month.

Previous calculations concerning the volume of Level II data (CCD/558) showed that a 60-socond recording of F waves sampled 20 tines por second on a vertical SP instrument would amount to 1,2C0 computer words, and a 20-ninute three-component recording of surface waves sampled once a second would amount to $3,600$ computer words. As an extension to the earlier recommendations, however, it would seem advisable to include, in addition to the vaveforms of P and L waves, snall segments of the noise preceding the signals. In the case of SPZ instruments, a 30-second noise segment should be taken, and in the case of LPZ instruments, a five-minute segment. In this case, a 90-second recording on a SP instrument together with a 25-ninute recording on a Z component and a 20-ninute recording on each of two horizontal LP instrument will amount to 5,700 words, or slightly nore if auxiliary information is taken into account. Thus, the total volume of Level II data for five events per month from 25 stations equipped with digital recording devices would be approximately 712,500 words. The remaining 25 stations in the assumed global network do not have digital recording facilities and would therefore transmit Level II information in analog form and not over digital channels.

It is also possible to estimate the approximate volume of data to be stored in a center subsequent tc the processing of Level I data.

In accordance with the proposed format for catalogues of seismic events, one event requires approximately 30 computer words. If it is assumed that, over a 24-hour period, a center detects *^0* events, each of which is recorded by half the stations in the global network, i.e. 25 stations, the volume of focal-parameter data over a 24-hour period will be: $50 \times 50 = 1,500$ words. The volume of azimuth and epicentral distance data for the 50 events detected by array stations over a 24-hour period will be 50 x 25 x 2 = 2,500. Thus, the total volume will be 4,000 words.

If it is assumed that all Level I data received by a center are transferred to the bank for long-term storage (some of the data will be associated with located events, while the rest will consist of unassociated signals), the volume of data received by the bank over a 24-hour period will be: $156,300 + 4,000 = 160,300$ words. **CD/43 Add. 1 page** 96

 $\mathcal{L}_{\rm{max}}$

 $\sim 10^{-1}$

Since Level I data and the focal parameters of events \;ill have to he stored in the center over a long period, an estimate should be made of the volume of data **that may he expected in this connection.**

In the course of one month, the total volume of Level I data, processed data and data concerning instrument calibration parameters would be approximately **5 million vrords , so that in the course of one year, the volume of data would be** about 60 million words.

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АРРЕ1Ш1К 6.9

Specification of the equipment to be used at International Data Centers

This appendix contains a brief description of the equipment needed at the individual international data centers to carry out the tasks specified for such centers. This question is also addressed in the first report of the Ad hoc group $(CCD/558)$.

International centers in the global network must be equipped to receive data through MMO channels and to process, analyze and store both reported and processed data. In this connection, the centers must be provided with sufficiently powerful modern computers and communication equipment.

The report of the Ad hoc group (CCD/558) suggests that centers should be equipped as follows.

Each center should have a main computer, which would process Level I data, and two mini-computers, one of which would assure communication between the center and stations in the global network and between centers, and the other of which would perform back-up functions. The data center's mann computer could include the following.

A central processor with a memory that can store at least 100,000 computer words and a calculating speed of at least one million instructions per second. Mass storage on disk for data and programs, with a capacity of at least 50 million computer words.

Four magnetic tape transports for digital recording.

Three interactive terminals.

Access to a large back-up computer (either nearby or remote) in case of a system breal:dovm.

The data archive function will require another computer with a large memory.