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Working Party on the Transport of Dangerous Goods<br>Joint Meeting of the RID Safety Committee and the Working Party on the Transport of Dangerous Goods<br>(Geneva, 14-24 September 1999<br>Bern, 20-24 March 1999)

AMENDMENTS TO CLASS 2

UN 1959, 1965, 3220, 3337, 3338, 3339, 3340
Submitted by the Expert from Italy

DIFLUOROETHYLENE - item $2^{\circ} \mathrm{F}$ - UN 1959 (REFRIGERANT GAS R1132a)
Proposal 1.1
In Supplement No. 1 / Alphabetic list delete "Vinylidene fluoride - $1959-2-2^{\circ} \mathrm{F}$ ".

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## Justification

The name "Vinylidene fluoride" is not the official name given in marginal $2201 / 201$, and it is no longer an accepted synonym as it was until the 1995 editions of RID/ADR.

## HYDROCARBON GAS MIXTURE, LIQUEFIED, N.O.S. - item $2^{\circ}$ F, UN 1965 -MIXTURE B1

## Proposal 2.1

In the tables of marginal 2201 / 201 replace "... 2.3 MPa (23 bar)" with "... 2.6 MPa (26 bar)".

## Justification

The mixtures B 1 and B 2 are two new groups of mixtures originating from mixture B , introduced for the first time in the 1999 edition of RID/ADR.

The main difference among the 3 mixtures is the density at $50^{\circ} \mathrm{C}$.
As shown in marginal $2250 / 250$, the mixtures B, B1 and B2 have the same test pressure for receptacles.
Since this test pressure is calculated, according to marginal 2219(d)/219(d), on the basis of the value of vapour pressure at $70^{\circ} \mathrm{C}$ minus 100 kPa , this means that also the values of the three vapour pressures at $70^{\circ} \mathrm{C}$ given in marginal 2201 / 201 must be the same ( 2.6 MPa ).

This is confirmed also by the identity of the test pressures for shells, with or without thermal insulation, given in marginals $211251 / 2.5 .2 .5$ and $212251 / 2.5 .2 .5$, which are based on vapour pressures at $65^{\circ} \mathrm{C}$ and $60^{\circ} \mathrm{C}$.

## PENTAFLUOROETHANE - item $2^{\circ}$ A - UN 3220 (REFRIGERANT GAS R 125)

## Proposal 3.1

In the tables of marginal $2250 / 250$ change in the first line the value of the pressure test corresponding to the filling degree of $0.95 \mathrm{~kg} / \mathrm{l}$ from " 3.4 MPa " to " 4.9 MPa ".

## Justification

The value of the critical temperature for Pentafluoroethane is $66.3^{\circ} \mathrm{C}$.
According to marginal 2219(c) / 219(c) the filling degree shall be such that the internal pressure at $65^{\circ} \mathrm{C}$ does not exceed the test pressure.

Owing to the proximity to the critical temperature the variation of the vapour pressure at $65^{\circ} \mathrm{C}$ with the filling degree is extremely high.

Data published by D. R. Defibaugh and G. Morrison "Compressed Liquid Densities and Saturation Densities of Pentafluoroethane (R125)" show the following internal pressures for different filling degrees in the region of $65^{\circ} \mathrm{C}$ :

| Temperature $\left({ }^{\circ} \mathrm{C}\right)$ | Pressure $(\mathrm{kPa})$ | Density $(\mathrm{kg} / \mathrm{l})$ |
| :--- | :---: | :---: |
| 65.882 | 3816.3 | 0.8179 |
| 65.895 | 4067.3 | 0.8613 |
| 65.885 | 4547.7 | 0.9098 |
| 65.874 | 5069.3 | 0.9440 |
| 65.880 | 5535.5 | 0.9671 |
| 65.885 | 6168.6 | 0.9922 |

The pressure test of 3.4 MPa given in marginal 2250/250 of the 1999 edition of RID/ADR is not correct and is unsafe, and is recommended that the value of 4.9 MPa given in the 1997 edition of RID/ADR be used.

This value is near the values indicated below of 5069.7 kPa at a temperature of $65.874^{\circ} \mathrm{C}$ with a filling degree of $0.9440 \mathrm{~kg} / \mathrm{l}$.

## 4. REFRIGERANT GAS R 404 A - item $2^{\circ}$ A - UN 3337 <br> REFRIGERANT GAS R 407 A - item $2^{\circ}$ A - UN 3338 <br> REFRIGERANT GAS R 407 B - item $2^{\circ}$ A - UN 3339 <br> REFRIGERANT GAS R 407 C - item $2^{\circ}$ A - UN 3340

## Proposal 4.1

In the tables of marginals $2250 / 250,211251 / 2.5 .2 .5$ and $212251 / 2.5 .2 .5$ change the maximum filling degree for:

| - | Refrigerant gas R 404 A | from | $" 0.82 \mathrm{Kg} / \mathrm{l} "$ | to | $" 0.84 \mathrm{Kg} / \mathrm{l} "$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| - | Refrigerant gas R 407 A | from | $" 0.94 \mathrm{Kg} / \mathrm{l} "$ | to | $" 0.95 \mathrm{Kg} / \mathrm{l} "$ |
| - | Refrigerant gas R 407 B | from | $" 0.93 \mathrm{Kg} / \mathrm{l} "$ | to | $" 0.95 \mathrm{Kg} / \mathrm{l} "$ |

## Justification

The values given in ADR / RID are based on the UN publication "Transport of dangerous goods Rev.10", originating from ST/SG/AC.10/C.3/R. 774 dated 25 April 1996.

The data sheets attached to this document show the following values of density at $50^{\circ} \mathrm{C}$ :

```
- R 404 A 0.89 Kg/l
- R 407 A 1.00 Kg/l
- R 407 B 1.00 Kg/l
```

Therefore according to marginals 2219 (d) / 219 (d), 211251 (3) / 2.5.2.3 and 212251 (3) / 2.5.2.3 the maximum filling degrees are:

| - | R 404 A | $0.95 \times 0.89=0.84$ |
| :--- | :--- | :--- |
| - | R 407 A | $0.95 \times 1.00=0.95$ |
| - | R 407 B | $0.95 \times 1.00=0.95$ |

## Note

This proposal will also be submitted to the UN Sub-Committee of Experts to be incorporated in the next revision of the publication "Transport of Dangerous Goods".
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## Proposal 4.2

In the tables of marginal 2250 / 250 change the values of the test pressures as follows:

| - R 404 A | from | "3.6 MPa" | to | $" 3.5 \mathrm{MPa} "$ |
| :--- | :--- | :--- | :--- | :--- |
| - R 407 A | from | "3.6 MPa" | to | $" 3.5 \mathrm{MPa} "$ |
| - R 407 B | from | "3.8 MPa" | to | $" 3.7 \mathrm{MPa} "$ |
| - R 407 C | from | "3.5 MPa" | to | $" 3.4 \mathrm{MPa} "$ |

## Justification

The values of the vapour pressures at $70^{\circ} \mathrm{C}$ from the calculation program "NIST THERMODYNAMIC PROPERTIES OF REFRIGERANTS AND REFRIGERANT MIXTURES (Rev. 5.10)" are:

| - | R 404 A | 3.60 MPa | rounded up to | 3.6 |
| :--- | :--- | :--- | :--- | :--- |
| - | R 407 A | 3.57 MPa | rounded up to | 3.6 |
| - | R 407 B | 3.75 MPa | rounded up to | 3.8 |
| - | R 407 C | 3.41 MPa | rounded up to | 3.5 |

Therefore the values of the test pressure, according to marginal 2219 (d)/219 (d), should be

| - | R 404 A | 3.5 MPa |
| :--- | :--- | :--- |
| - | R 407 A | 3.5 MPa |
| - | R 407 B | 3.7 MPa |
| - | R 407 C | 3.4 MPa |

## Note

This proposal will also be submitted to the UN Sub-Committee of Experts to be incorporated in the next revision of the publication "Transport of Dangerous Goods".

## Proposal 4.3

In the tables of marginals $211251 / 2.5 .2 .5$ and $212251 / 2.5 .2 .5$ change the minimum test pressures for shells with thermal insulation relevant to:

and change the minimum test pressures for shells without thermal insulation relevant to:

| - | Refrigerant gas R 407 A | from | $" 3.3 \mathrm{MPa} "$ | to | $" 3.2 \mathrm{MPa} "$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| - | Refrigerant gas R 407 B | from | $" 3.4 \mathrm{MPa} "$ | to | $" 3.3 \mathrm{MPa} "$ |
| - | Refrigerant gas R 407 C | from | "3.1 MPa" | to | $" 3.0 \mathrm{MPa} "$ |

## Justification

The values given in ADR / RID are based on the UN publication "Transport of dangerous goods - Rev. 10", originating from ST/SG/AC.10/C.3/R. 774 dated 25 April 1996.

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The data sheets attached to this document show the following values of vapour pressures:

|  | at $60^{\circ} \mathrm{C}$ | at $65^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| - | R 407 A | 2.90 MPa |
| - | R 407 B | 3.05 MPa |
| - | R 407 C | ---- |

Therefore according to marginals $211251(3) / 2.5 .2$. 3 and $212251(3) / 2.5 .2 .3$ the test pressures for shells with thermal insulation are:

- R 407 A
$2.9-0.1=2.8 \mathrm{MPa}$
- R 407 B
$3.1-0.1=3.0 \mathrm{MPa}$
and for shells without thermal insulation

| - | R 407 A |
| :--- | :--- |
| - | R 407 B |
| - | R 407 C |


[^0]:    */ Distributed by the Central Office for International Carriage by Rail (OCTI) under the symbol OCTI/RID/GT-III/1999/32.

